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CO LTD

(22)Date of filing : 25.12.1992 (72)Inventor : TAKEUCHI MICHIKO

MASUBUCHI NOBORU

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(54) LENTICULAR LENS, SURFACE LIGHT SOURCE AND LIQUID CRYSTAL  
DISPLAY DEVICE

(57)Abstract:

PURPOSE: To enable a bright surface light emission to be realized, and to condense a diffused light within a prescribed angle range in the vicinity of a normal line without increasing power consumption and a heat-generating value by providing a unit concave lens part whose cross section is a circular shape.

CONSTITUTION: In a lenticular lens 10, one face of a translucent substrate 11 is made as a lens 12 on which many unit concave lens parts 12-i ( $i=1-N$ ) whose cross section is a circular shape, etc., are formed so that the major axis (edge) directions become parallel to each other, and the other face of the translucent substrate 11 is made as a flat face 13. Also, in the unit concave lens part 12-i of the lens face 12, a shape of a main cutting plane cut by a cross section being vertical to the major axis (edge) is a shape obtained by extracting and using a secondary curve of circular shape, an elliptical shape, a hyperbola, a parabola, etc., or a Rankine body, a curve shown by a single-valued function of trochoid,

cycloid, cardioid, involute, etc., and also, a part (usually being under a semicircle) of a curve being similar thereto, smooth and continuous, and being concave or convex in one direction.

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#### CLAIMS

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[Claim(s)]

[Claim 1]A lenticular lens having the formed lens side so that a major axis direction may become parallel mutually about unit concave lens parts, such as round cross section shape, in one field of a translucency substrate, and having a flat face in a field of another side of said translucency substrate.

[Claim 2]A lenticular lens comprising:

A translucency substrate with which both sides were formed in a flat face.

A lens layer which consists of translucency material which was laminated by one field of said translucency substrate, and formed many unit concave lens parts, such as round cross section shape, so that a major axis direction might become parallel mutually.

[Claim 3]The lenticular lens according to claim 1 or 2 [ either / both sides or ] said translucency substrate or said lens layer having optical isotropic diffusion nature, or forming direction diffusibility layers, such as light, in one side of said translucency substrate or said lens layer.

[Claim 4]A transparent material which consists of a cave of a translucency plate or rectangular parallelepiped shape, and a linear light source adjoined and provided in both sides or one side of a side edge of said transparent material, The surface light source, wherein the surface of said lenticular lens becomes any 1 paragraph of direction diffusibility layers, such as light laminated on the surface of said transparent material, and said claim 1 - claim 3 with a diffused-light emission surface including a lenticular lens of a statement.

[Claim 5]One or more punctiform or linear light sources and a lamp house which surrounded said light source and used the 1st page as an opening, The surface

light source, wherein it covers said opening and the surface of said lenticular lens becomes any 1 paragraph of said claim 1 - claim 3 with a diffused-light emission surface including a lenticular lens of a statement.

[Claim 6]A liquid crystal display comprising:

A transmission type liquid crystal display element.

Said surface light source according to claim 4 or 5 provided in the back of said liquid crystal display element.

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## DETAILED DESCRIPTION

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[Detailed Description of the Invention]

[0001]

[Industrial Application]This invention relates to the lenticular lens which formed many unit lens parts so that a major axis direction might become parallel mutually, the surface light source using the lenticular lens, and the liquid crystal display using the surface light source as a back light.

[0002]

[Description of the Prior Art]The thing using the direct bottom part or the edge light type diffusing surface light source as a liquid crystal display is known

(JP,2-284102,A, U.S. Pat. No. 4729067, JP,63-318003,A, JP,3-92601,A, etc.).

[0003]Drawing 15 is a figure showing the conventional example of the edge light type surface light source. As for the surface light source 100A, the direction [ field / of the translucency board 101 / one ] light diffusibility layer 102 is formed, and the reflecting layer 103 is formed in the field of another side.

The punctiform or linear light source 104 is arranged on the side.

As for the surface light source 100B, the triangle-pole-prisms type lenticular lens 105 whose vertical angle is 90 degrees is further formed on the direction light diffusibility layers 102, such as the surface light source 100A.

[0004]

[Problem(s) to be Solved by the Invention]As for the former surface light source 100A, uniform and isotropic luminescence is obtained by the method light diffusibility layer 102 of \*\*. However, since light energy was released even to the practically unnecessary oblique position or the tangential direction of the luminescence (light emission) side, the loss of the light energy released near [ very required ] the normal line direction (they are [ as opposed to / in general / a normal ] 30 degrees - 0 times [ 90 / or less ] or more) increased, and there was a problem that energy efficiency was bad.

[0005]Since the light isotropic diffusion was carried out [ light ] by the method light diffusibility layer 102 of \*\* is deflected by the prism action of the lenticular

lens 105, light energy concentrates near the normal line direction, the latter surface light source 100B has the high utilization efficiency of energy, and a rise in luminosity is possible for it at low power consumption. However, the phenomenon (side lobe in the angular distribution of transmitted light intensity) in which a part of lights deviated from the predetermined angle range near the normal line direction occurred, and there was a problem that the light emitted to the oblique position turned into unnecessary light (the stray light, optical noise) to a neighboring worker.

[0006]Without solving the above-mentioned technical problem and increasing power consumption and calorific value in liquid crystal display, bright surface light is possible for the purpose of this invention, and it is providing the lenticular lens, the surface light source, and the liquid crystal display which can condense the diffused light to the predetermined angle range near the normal moreover.

[0007]

[Means for Solving the Problem]This invention solves said technical problem by the following solving means. In order to understand easily, numerals corresponding to an example are attached and explained, but it is not limited to this.

[0008]Namely, the 1st solving means of a lenticular lens by this invention, It has the formed lens side (12) so that a major axis direction may become parallel

mutually in one field of a translucency substrate (11) about unit concave lens parts (12i), such as round cross section shape, and it has a flat face (13) in a field of another side of said translucency substrate.

[0009]This invention is characterized by the 2nd solving means of a lenticular lens comprising the following.

A translucency substrate (14) with which both sides were formed in a flat face.

A lens layer (15) which consists of translucency material which was laminated by one field of said translucency substrate, and formed many unit concave lens parts, such as round cross section shape, so that a major axis direction might become parallel mutually.

[0010]The 3rd solving means of a lenticular lens by this invention, In said 1st or 2nd solving means, [ either / both sides or ] said translucency substrate or said lens layer has optical isotropic diffusion nature, or direction diffusibility layers (20, 20), such as light, are formed in one side of said translucency substrate or said lens layer.

[0011]The 1st solving means of the surface light source by this invention, A linear light source (43) adjoined and provided in both sides or one side of a side edge of a transparent material (41) which consists of a cave of a translucency plate or rectangular parallelepiped shape, and said transparent material, The



surface of said lenticular lens turns into a diffused-light emission surface including a lenticular lens (10) by either [ direction diffusibility layers (20), such as light laminated on the surface of said transparent material, and ] said 1st [ the ] - the 3rd solving means.

[0012]The 2nd solving means of the surface light source by this invention One or more punctiform or linear light sources (32), Said light source is surrounded, a lamp house (31) which used the 1st page as an opening, and said opening are covered, and the surface of said lenticular lens turns into a diffused-light emission surface including a lenticular lens (10) by either said 1st [ the ] - the 3rd solving means.

[0013]It is characterized by a solving means of a liquid crystal display of \*\* comprising the following in this invention.

A transmission type liquid crystal display element.

The surface light source by said 1st or 2nd solving means provided in the back of said liquid crystal display element (30, 40).

[0014]

[Function]In this invention, the lenticular lens has unit concave lens parts, such as round cross section shape.

Therefore, the diffused light which passed along the direction light diffusibility

layer etc. condenses in the angle range of the request near the normal.

Therefore, the angular distribution of the diffused-light intensity emitted from a diffused-light emission surface turns into almost uniform isotropic distribution only in a desired angle range, And a side lobe stops occurring and it can be used conveniently for the surface light sources, such as a direct lower part type or an edge light system, the liquid crystal display using them, etc.

[0015]

[Example] Hereafter, with reference to drawings etc., this invention is explained in detail about an example.

(Example of an integral-type lenticular lens) Drawing 1 is a figure showing the 1st example of the lenticular lens by this invention, drawing 1 (A) is a perspective view and drawing 1 (B) is a X-X sectional view. The lenticular lens 10 of the 1st example makes unit concave lens part 12-i ( $i=1-N$ ), such as round cross section shape, the formed lens side 12 in one field of the translucency board 11 so that the direction of a major axis (\*\*) may become parallel mutually, and it makes the field of another side of the translucency board 11 the flat face 13.

[0016] The translucency substrate 11, Independent or transparent resin of acrylic ester, such as methyl polymethacrylate and poly(methyl acrylate), or methacrylic acid ester, such as polyester, such as a copolymer, polyethylene terephthalate, and polybutylene terephthalate, polycarbonate, and polystyrene, etc. It is the

sheet shaped or tabular member which carried out the flat surface or curving surface shape which consists of translucency materials, such as transparent ceramics, such as (what carried out bridge construction hardening with thermoplastics or heat, ultraviolet rays, and an electron beam), and transparent glass. It is water-white, and also it is necessary to select it so that the diffused light may be penetrated at worst, and it may be coloring transparency or lusterless transparency to such an extent that the translucency required of this translucency substrate 11 does not have trouble in use of each use. Here, lusterless transparency means the character to which the diffuse transmission of the transmitted light is made to carry out in all the directions of [ within a half-solid angle ] isotropic almost uniformly, and it is used for optical isotropic diffusion nature and synonymous words. As for the translucency substrate 11, when using as an object for the sources of back light, thickness is about 20-1000 micrometers, and it is preferred to use the thing of plane shape. However, a direct bottom part or a transparent material may be a cave, and it may be a case where direction diffusibility layers, such as light, are flexible thin sheets, and in order to hold the shape of a light emission side, when using thicker resin, it may be about 1-10 mm about thickness.

[0017]The shape of the main cutting plane cut by the section vertical to a major axis (\*\*) unit concave lens part 12-i of the lens side 12 Secondary curves, such

as circular, an ellipse form, a hyperbola, and a parabola, or similar to the curve expressed with univalent functions, such as a Rankine's oval, a trochoid, a cycloid, cardioid, and involute, and these other -- it is smooth and is continuing. It is the shape where a part of curve (it is called circular shape etc.) (usually less than a semicircle) used as concave or a convex was extracted and used in the one direction.

The angular distribution as a diffused-light emission surface is determined by shape parameters, such as the curvature radius  $r$ , the amount  $D$  of cuts, and the cycle  $P$ , and, as for unit concave lens part 12-i, about about 20-1000 micrometers is preferred respectively. Direction of the lens side 12 may be any by the side of a light source and light emission (the light source side and an opposite hand). [Refer to drawing 9 and drawing 10.] .

[0018]A heat pressing method the lens side 12 is publicly known, for example (JP,56-157310,A statement), After carrying out embossing to the thermoplastic resin film of ultraviolet curing nature by a roll embossing plate, it can fabricate by the method (JP,61-156273,A statement) of irradiating with ultraviolet rays and stiffening the film etc.

[0019](Example of the lenticular lens of a lamination type) Drawing 2 is a sectional view showing the 2nd example of the lenticular lens by this invention. Although the lenticular lens 10 of the 1st example is formed and carried out with

the simple substance of the translucency substrate 11, lenticular lens 10' of the 2nd example is the structure which laminated the lens layer 15 which consists of translucency material which has the lens side 12 of the same shape as the above-mentioned on the flat translucency board 14. A process carries out coating of an electron beam or the ultraviolet-curing-resin liquid to a roll (cylinder)-like mold, Where a transparent substrate sheet is further stuck on a coating surface, after stiffening resin liquid, the methods (U.S. Pat. No. 4576850, U.S. Pat. No. 3689346, JP,3-223883,A, etc.) of releasing from mold the hardening resin by which pasted up the substrate sheet on this and the allocated type was carried out in the uneven shape of the mold -- therefore, it manufactures.

[0020](Shape of a unit concave lens part) Drawing 3 is a sectional view showing the shape of the unit concave lens part of the lenticular lens by an example. If an elliptical cross section-like case is mentioned as an example, as shown in drawing 3 (A), unit concave lens part 12-i, for example, The flat part 12b may be formed in a summit, and it may be made to form the smooth surface part 12c in a summit, as it may have the acumination part 12a in which the summit sharpened using a part of ellipse, and it is shown in drawing 3 (B), and shown in drawing 3 (C).

[0021](Locus of a beam of light) Drawing 4 - drawing 7 are the figures showing

the locus of a beam of light which passes the lenticular lens by an example. The beam of light which entered into the lenticular lens 10 is the curvature radius  $r$ , the amount  $D$  of cuts, and the cycle  $P$  of a lens. [Refer to drawing 1 (B).] And it is emitted by the predetermined angular distribution decided by the refractive index  $n$  etc. The lenticular lens 10 of drawing 4 and drawing 7 makes an example curvature-radius [ equivalent to the example 1 of manufacture mentioned later / of  $r = 35$  micrometers ], pitch [ of  $P = 59$  micrometers ], amount [ of  $D = 15$  micrometers ] of cuts, and refractive-index  $n_1 = 1.5$  (acrylic resin), and carries out a simulation.

[0022]The optimization design of parameter  $n_1$  for obtaining desired diffusion angle  $\theta_s$ ,  $P$ , and  $D$  is performed as follows. Like the source of back light of a direct bottom part, when most incident light enters into the flat face 13 at a right angle (incidence angle = 0 degree), it is decided by where the part by which a total reflection condition is fulfilled in general becomes. In drawing 4, an angle of refraction becomes large and a total reflection condition is exactly greeted between beam-of-light  $R_2$  and  $R_3$  and between beam-of-light  $R_9$  and  $R_{10}$  as a beam of light goes around a lens. Beam-of-light  $R_{2.5}$  at this time and  $R_{9.5}$ , Eject to the tangential direction of a lens and the beam of light outside this, It changes from sending light to convergence light quickly like  $R_1$  and  $R_{11}$  again as it will be very small and will go outside for a while rather than this, if it sees from the whole

light volume, although there are some which spread greatly like  $R_2$  and  $R_{10}$  in part. Therefore, supposing the range (between beam-of-light  $R_{2.5}$  and  $R_{9.5}$ ) until a beam of light causes total internal reflection becomes diffusion angle  $\theta_s$  of radiated light in general, it will become like drawing 5 and drawing 6.

[0023]\*\* In amount  $D \leq r \sin \theta_c$  cuts  $\theta_c$  (it becomes total internal reflection by either), when a section is a circle, don't depend at the situation of a curvature radius, but it is  $\theta_s = 180 - \theta_c = \sin^{-1}(1/n_1)$ .

Since it became, when desired  $\theta_s$  is given, it is  $n_1 = 1/(\sin \theta_s)$ .

\*\* -- refractive-index  $n_1$  of a lens can be chosen like.

[0024]\*\* In the case of amount  $D > r \sin \theta_c$  cuts  $\theta_c > 0$  (always with  $[\theta < \theta_c]$  no total internal reflection), it is  $n_1 \sin \theta_1 = n_2 \sin \theta_2$  therefore  $\theta_2 = \sin^{-1}(n_1 \sin \theta_1)$ .

A diffusion angle is profile  $\theta_s = 2(\theta_2 - \theta_1) = 2$  from  $\theta_1 = \tan^{-1}(x/D)$ .

$$[\sin^{-1}\{n_1 \sin(\tan^{-1}(x/D))\} - \tan^{-1}(x/D)]$$

It becomes. When it has an acuminant part like drawing 3 (A) especially, it is  $\theta_s = 2$  from  $2x = P$ .  $[\sin^{-1}\{n_1 \sin(\tan^{-1}(P/2D))\} - \tan^{-1}(P/2D)]$

Since it becomes, when desired  $\theta_s$  is given, refractive-index  $n_1$  of a lens, the amount  $D$  of cuts, and the cycle  $P$  can be chosen, and the degree of option increases so that it may become the aforementioned  $\theta_s$ .

[0025]Drawing 4 is the direct bottom part surface light source. like the light

source right above part of [refer to drawing 11], to the flat face 13 of the lenticular lens 10, it enters as an incidence angle  $=0$  degree parallel pencil, and signs that it emanates from the concave lens part 12 are boiled, and it is shown.

[0026]Drawing 7 is an edge light mold face light source. It is a case where laid the lenticular lens 10 on the direction diffusibility layers 20, such as light of [refer to drawing 12], and light is entered from the flat face 13, and signs that the light flux distributed over a certain angle range (it is the range of  $-40$  degrees -  $+40$  degrees to the normal N at drawing 7) entered are shown. [Refer to drawing 13 (C).]

[0027](Direction diffusibility layers, such as light) Drawing 9 and drawing 10 are the figures showing lamination with direction diffusibility layers, such as a lenticular lens, light, etc. concerning an example. The lenticular lens 10 and the direction diffusibility layers (lusterless hyaline layer) 20, such as light, can be laminated and used. In this case, in order to once complete the light diffused by the direction diffusibility layers 20, such as light, a lenticular lens 10 observation-side needs to arrange the direction diffusibility layers 20, such as light, to the light source side.

[0028]As mentioned above, even if the lens side 12 of the lenticular lens 10 is an observation side It may be by [drawing 9 (A) and drawing 10 (A)], or may be a light source side. [Refer to drawing 9 (B) and drawing 10 (B).] The direction



diffusibility layers 20, such as light, are sheet (or board)-like things. The thing of the shape of a film which was good also as for [refer to drawing 9], and carried out coating to the lenticular lens 10 directly like direction diffusibility layer 20', such as light [Also referring to drawing 10] is good.

[0029]In the direction diffusibility layers 20 and 20, such as light, as a light diffusion agent (flatting agent) into said translucency material Minerals particles, such as calcium carbonate, silica, alumina, and barium sulfate, Or what distributed resin-beads particles, such as an acrylic resin, is used, and, as for the path of the particle, the thing like abbreviated 1-20micrometer is used. The direction diffusibility layers 20, such as light, can use a formation thing for said translucency material as a monolayer which sheet-ized the resin material which scoured said light diffusion agent by extrusion molding, calender molding, etc. The two-layer structure which used the paint which made this distribute said light diffusion agent by using said translucency material as a binding material (binder) on the sheet (or board) of said translucency material having carried out coating formation may be sufficient. What formed the fine irregularities (grain etc.) of 1-20 micrometers of arithmetical mean deviation of profile for the surface of the sheet (or board) of said translucency material by sandblasting, embossing Chinese poem type processing, etc. may be used.

[0030](Example of the surface light source of a direct bottom part) Drawing 11 is

a sectional view showing the 1st example (direct bottom part) of the surface light source by this invention. As for the surface light source 30 of the direct bottom part, the line light source 32 of a fluorescent lamp etc. is established in the case 31.

The direction diffusibility layers 20, such as light, and the lenticular lens 10 are formed in the opening side of the case 31.

[0031](Example of the edge light type surface light source) The deployment perspective view and drawing 13 in which the 2nd example (edge light type) of the surface light source according [ drawing 12 ] to this invention is shown are a figure for explaining the characteristic of a light guide plate. As for the edge light type surface light source 40, the reflecting layer 42 is formed in the undersurface of the light guide plate 41.

The direction diffusibility layers 20, such as light, and the lenticular lens 10 are arranged at the upper surface of the light guide plate 41.

The light source 43, the reflection film 44, and the illuminating cover 45 are formed in the both sides of the side edge of the light guide plate 41, respectively.

[0032]In being larger than the critical angle  $\theta_c$ , it is only spreading, while a beam's of light carries out total internal reflection of the inside of the light guide plate 41, as shown in drawing 13 (A), and the transmitted light from the emission

surface 41a does not have the incidence angle  $i$  of the light guide plate 41. On the other hand, when smaller than the critical angle  $i_c$ , as shown in drawing 13 (B), in the side interface of the emission surface 41a of the light guide plate 41, a part of beam of light is reflected (the inside of the light guide plate 41 is spread), the remainder penetrates and the incidence angle  $i$  is emitted. In the actual light guide plate 41, as shown in drawing 13 (C), by putting light source 43' on the end face of another side, or providing light reflection layer 42', a beam of light spreads the inside of the light guide plate 41 bidirectionally, and light is emitted in the symmetrical direction of  $\theta$  to a normal.

[0033](Example of a light reflection layer) Drawing 14 is a figure showing the example of the light reflection layer used for the edge light type surface light source. The light reflection layer 42 is a layer with the performance to which diffuse reflection of the light is carried out, and can be constituted as follows.

\*\* Form the white layer 42A which made one side of the light guide plate 41 distribute powder, such as high concealment nature and paints with a high whiteness degree, for example, a titanium dioxide, and aluminum, by paint etc. like drawing 14 (A).

\*\* Like drawing 14 (B), by sand bright processing, embossing, etc., form the lusterless detailed unevenness 41a, and further, plating or vacuum evaporation makes metal, such as aluminum, chromium, and silver, one side of the light

guide plate 41, and form the metallic thin film layer 42B in it.

\*\* Form the metallic thin film layer 42B in the same white layer 42A' (however, concealment nature may be low) as drawing 14 (A) like drawing 14 (C).

\*\* It may be made to amend that form white layer 42A" of dot shape, increase an area rate as it keeps away from the light source 43 as shown in drawing 14 (D1) and (D2), and the light volume of the light source 43 declines.

[0034]The surface light sources 30 and 40 shown in drawing 11 and drawing 12 can be used as a liquid crystal display by arranging at the back of a transmission type publicly known liquid crystal display element. It is applicable to the element which needs sources of back light other than a transmission type liquid crystal display element, such as an electrochromic display device.

[0035](Transit measurement) This artificer produces a lenticular lens as shown in the examples 1 and 2 of manufacture, and the comparative example 1, and it is made for lens side 12 grade to turn to the edge light mold face light source 40 shown in drawing 12 up (outside), It laid on the direction diffusibility layers 20, such as light, and the angular distribution of the luminosity of the light emitted from lens side 12 grade was measured. Only also in the direction diffusibility layers 20, such as light, it measured as the comparative example 2.

[0036]Example of manufacture 1 shape ; Drawing 1 (or drawing 2) and a section are the circular curvature radii  $r$ ; 35micrometer cycle  $P$  ; The amount  $D$  of

59micrometer cuts ; 15micrometer material ; Acrylic resin refractive-index  $n_1$ ;

The shape of example dimorphism of 1.5 manufactures ; Drawing 3 (B), A

section is the circular curvature radius  $r$ ; 100micrometer cycle P ; The amount D

of 300micrometer cuts ; 100micrometer material ; Acrylic resin refractive-index

$n_1$ ; 1.5 comparative-example 1 shape ; Vertical-angle =90 degree, both basic

angles = 45-degree 3 square-pillar prism type lenticular lens [Drawing 15 (B)]

Cycle P ; 100micrometer material ; Acrylic resin refractive-index  $n_1$ ; They are the

direction diffusibility layers 20, such as light, without using 1.5

comparative-example 2 lenticular lens. It measured by [drawing 15 (A)].

[0037]The measurement result of the examples 1 and 2 of manufacture and the

comparative examples 1 and 2 is shown in the curve A, B, and C of drawing 8,

and D, respectively. The following table 1 is obtained based on these

measurement results.

Table 1 (measurement result)

Half angle  $\theta_{H[**]}$  Side lobe ratio[%] Normal line direction luminance ratio [%]

Example 1 of manufacture; 38 11 Example 2 of 111.2 manufactures; 35 22

108.5 comparative examples 1; 34 26 135.0 comparative examples 2; 37 0

100.0 (standard)

[0038]As for it, if drawing 8 or Table 1 is referred to, the examples 1 and 2 of

manufacture turn out that the diffused light is condensed by the prescribed range

near the normal line direction (usually half angle  $\theta_H = 30$  degrees - about 90 degrees) as compared with the case of only the mat layer 20 of the comparative example 2. As compared with the triangle-pole-prisms type lenticular lens of the 90-degree vertical angle of the comparative example 1, it turns out that there is little generating of side lobe light.

[0039]

[Effect of the Invention]As explained in detail above, according to this invention, the light of desired angular distribution can be diffused by the shape parameters (for example, a curvature radius, a cycle, the amount of cuts, a refractive index, etc.) of the unit concave lens part of the lens side of a lenticular lens (claims 1 and 2).

[0040]Therefore, since the diffused light is condensed by the desired angle range to a normal line direction by combining with direction diffusibility layers, such as light, like claim 3 as compared with the case of only direction diffusibility layers, such as light, In a predetermined angle range, even if it is the same power consumption, in order to become high-intensity more and to obtain the same luminosity conversely, low power consumption is more sufficient.

[0041]Since the light energy emitted to a tangential direction from an oblique direction decreases, generating of the stray light decreases more. As compared with the 3 square-pillar prism type lenticular lens of the conventional 90-degree

vertical angle, generating of side lobe light decreases and there is less generating of the stray light.

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## DESCRIPTION OF DRAWINGS

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[Brief Description of the Drawings]

[Drawing 1] It is a perspective view showing the 1st example of the lenticular lens by this invention.

[Drawing 2] It is a sectional view showing the 2nd example of the lenticular lens by this invention.

[Drawing 3] It is a sectional view showing the shape of the unit concave lens part of the lenticular lens by an example.

[Drawing 4] It is a figure showing the locus of a beam of light which passes the lenticular lens by an example.

[Drawing 5] It is a figure showing the locus of a beam of light which passes the lenticular lens by an example.

[Drawing 6] It is a figure showing the locus of a beam of light which passes the lenticular lens by an example.

[Drawing 7] It is a figure showing the locus of a beam of light which passes the

lenticular lens by an example.

[Drawing 8] It is a diagram showing the penetration characteristic of the example of the lenticular lens by this invention.

[Drawing 9] It is a figure showing lamination with direction diffusibility layers, such as a lenticular lens, light, etc. concerning an example.

[Drawing 10] It is a figure showing lamination with direction diffusibility layers, such as a lenticular lens, light, etc. concerning an example.

[Drawing 11] It is a sectional view showing the 1st example (direct bottom part) of the surface light source by this invention.

[Drawing 12] It is a deployment perspective view showing the 2nd example (edge light type) of the surface light source by this invention.

[Drawing 13] It is a figure for explaining the characteristic of the light guide plate shown in drawing 12.

[Drawing 14] It is a figure showing the example of the light reflection layer used for the edge light type surface light source.

[Drawing 15] It is a figure showing the conventional example of the edge light type surface light source.

[Description of Notations]

10 Lenticular lens

11 Translucency substrate



12 Lens side

13 Flat face

20 Direction diffusibility layers, such as light

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(72)発明者 竹内 道子

東京都新宿区市谷加賀町一丁目 1 番 1 号

大日本印刷株式会社内

(72)発明者 増淵 暢

東京都新宿区市谷加賀町一丁目 1 番 1 号

大日本印刷株式会社内

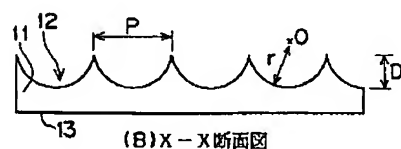
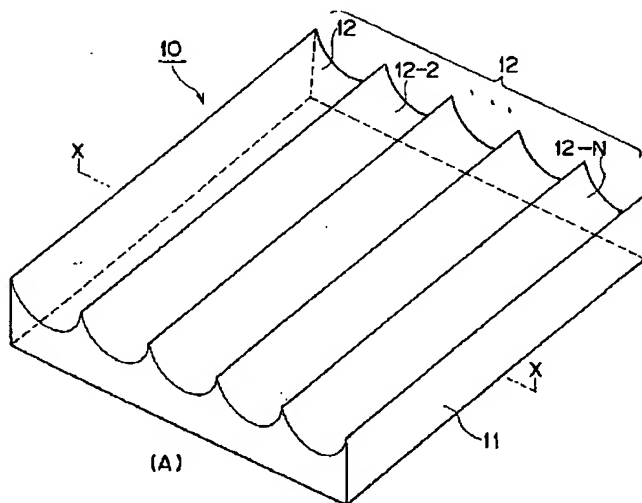
(74)代理人 弁理士 鎌田 久男

(54)【発明の名称】 レンチキュラーレンズ、面光源及び液晶表示装置

(57)【要約】

【目的】 消費電力や発熱量を増大させることなく、明るい面発光が可能であり、しかも、拡散光を法線近傍の所定の角度範囲に集光できる。

【構成】 透光性基材 1 1 の一方の面に断面円形状等の単位凹レンズ部 1 2 - 1 ~ 1 2 N を長軸方向が互いに平行になるように多数形成したレンズ面 1 2 を有し、透光性基材 1 1 の他方の面に平坦面 1 3 を有する。



O 曲率中心  
r 曲率半径  
D 切込量  
P 周期

(B) X-X断面図

## 【特許請求の範囲】

【請求項1】 透光性基材の一方の面に断面円形形状等の単位凹レンズ部を長軸方向が互いに平行になるように多数形成したレンズ面を有し、前記透光性基材の他方の面に平坦面を有することを特徴とするレンチキュラーレンズ。

【請求項2】 両面が平坦面に形成された透光性基材と、  
前記透光性基材の一方の面に積層され、断面円形形状等の単位凹レンズ部を長軸方向が互いに平行になるように多数形成した透光性材料からなるレンズ層とを含むことを特徴とするレンチキュラーレンズ。

【請求項3】 前記透光性基材又は前記レンズ層の双方又は一方が光等方拡散性を有するか、又は、前記透光性基材又は前記レンズ層の一方側に光等方拡散性層を形成することを特徴とする請求項1又は請求項2に記載のレンチキュラーレンズ。

【請求項4】 透光性平板又は直方体状の空洞からなる導光体と、  
前記導光体の側端面の双方又は一方に隣接して設けられた線状光源と、  
前記導光体の表面に積層した光等方拡散性層と、  
前記請求項1～請求項3のいずれか1項に記載のレンチキュラーレンズとを含み、  
前記レンチキュラーレンズの表面が拡散光放出面となることを特徴とする面光源。

【請求項5】 1以上の点状又は線状の光源と、  
前記光源を包囲し、1面を開口部としたランプハウスと、  
前記開口部を被覆し、前記請求項1～請求項3のいずれか1項に記載のレンチキュラーレンズとを含み、  
前記レンチキュラーレンズの表面が拡散光放出面となることを特徴とする面光源。

【請求項6】 透過型の液晶表示素子と、  
前記液晶表示素子の背面に設けられた前記請求項4又は請求項5に記載の面光源とを含むことを特徴とする液晶表示装置。

## 【発明の詳細な説明】

## 【0001】

【産業上の利用分野】本発明は、単位レンズ部を長軸方向が互いに平行になるように多数形成したレンチキュラーレンズ、そのレンチキュラーレンズを用いた面光源及びその面光源をバックライトとして用いた液晶表示装置に関するものである。

## 【0002】

【従来の技術】液晶表示装置として、直下型又はエッジライト型の拡散面光源を用いたものが知られている（特開平2-284102号、米国特許第4729067号、特開昭63-318003号、特開平3-9260

【0003】図15は、エッジライト型の面光源の従来例を示す図である。面光源100Aは、透光性基板101の一方の面に、等方光拡散性層102が形成され、他方の面に反射層103が形成されており、側面に点状又は線状の光源104が配置されたものである。また、面光源100Bは、面光源100Aの等方光拡散性層102の上に、さらに、頂角が90度の三角柱プリズム型のレンチキュラーレンズ105が形成されたものである。

## 【0004】

【発明が解決しようとする課題】前者の面光源100Aは、等方光拡散性層102により均一かつ等方的な発光が得られる。しかし、実用上不要な斜方向ないしは発光（光放出）面の接線方向にまで光エネルギーが放出されるので、真に必要な法線方向近傍（概ね、法線に対して0度以上30度～90度以下）に放出される光エネルギーの損失が多くなり、エネルギー効率が悪いという問題があった。

【0005】また、後者の面光源100Bは、等方光拡散性層102により等方拡散された光がレンチキュラーレンズ105のプリズム作用によって偏向されるので、法線方向近傍に光エネルギーが集中し、エネルギーの利用効率が高く、低消費電力で高輝度化が可能である。しかし、法線方向近傍の所定の角度範囲から一部の光が逸脱する現象（透過光強度の角度分布におけるサイドローブ）が発生し、斜方向に放出された光が近辺の作業者に対して不要光（迷光、光ノイズ）となる、という問題があった。

【0006】本発明の目的は、前述の課題を解決し、液晶表示において、消費電力や発熱量を増大させることなく、明るい面発光が可能であり、しかも、拡散光を法線近傍の所定の角度範囲に集光できるレンチキュラーレンズ、面光源及び液晶表示装置を提供することである。

## 【0007】

【課題を解決するための手段】本発明は、以下の解決手段によって、前記課題を解決する。なお、理解を容易にするために、実施例に対応する符号を付して説明するが、これに限定されるものではない。

【0008】すなわち、本発明によるレンチキュラーレンズの第1の解決手段は、透光性基材（11）の一方の面に断面円形形状等の単位凹レンズ部（12i）を長軸方向が互いに平行になるように多数形成したレンズ面（12）を有し、前記透光性基材の他方の面に平坦面（13）を有することを特徴とする。

【0009】本発明によるレンチキュラーレンズの第2の解決手段は、両面が平坦面に形成された透光性基材（14）と、前記透光性基材の一方の面に積層され、断面円形形状等の単位凹レンズ部を長軸方向が互いに平行になるように多数形成した透光性材料からなるレンズ層（15）とを含むことを特徴とする。

【0010】本発明によるレンチキュラーレンズの第3

【0019】（積層型のレンチキュラーレンズの実施例）図2は、本発明によるレンチキュラーレンズの第2の実施例を示す断面図である。第1の実施例のレンチキュラーレンズ10は、透光性基材11の単体で形成したものであるが、第2の実施例のレンチキュラーレンズ10'は、平坦な透光性基板14上に、前述と同様な形状のレンズ面12を有する透光性材料からなるレンズ層15を積層した構造である。製法は、ロール（円筒）状の型に電子線又は紫外線硬化樹脂液を塗工し、塗工面上に更に透明基材シートを密着させた状態で樹脂液を硬化させた後に、基材シートをこれに接着し、かつ、型の凹

特許第4576850号、米国特許第3689346号、特開平3-223883号等)によって製造する。

【0020】(単位凹レンズ部の形状)図3は、実施例によるレンチキュラーレンズの単位凹レンズ部の形状を示す断面図である。単位凹レンズ部12-iは、例えば、断面楕円形状の場合を例にあげると、図3(A)に示すように、楕円の一部を用いて頂上が尖った尖頭部12aを有していてもよいし、図3(B)に示すように、頂上に平坦部12bを形成してもよいし、また、図3(C)に示すように、頂上に滑らかな曲面部12cを形成するようにしてもよい。

【0021】(光線の軌跡)図4～図7は、実施例によるレンチキュラーレンズを通過する光線の軌跡を示す図である。レンチキュラーレンズ10に入射した光線は、レンズの曲率半径 $r$ 、切込量 $D$ 、周期 $P$ 〔図1(B)参照〕及び屈折率 $n$ などによって決まる所定の角度分布で放出される。図4及び図7のレンチキュラーレンズ10は、後述する製造例1に相当する曲率半径 $r=35\mu\text{m}$ 、ピッチ $P=59\mu\text{m}$ 、切込量 $D=15\mu\text{m}$ 、屈折率 $n_1=1.5$ (アクリル樹脂)を例にして、シミュレーションしたものである。

【0022】所望の拡散角 $\theta_s$ を得るためのパラメータ $n_1$ 、 $P$ 、 $D$ の最適化設計は以下のように行う。直下型の背面光源等のように、大部分の入射光が平坦面13に直角(入射角 $=0^\circ$ )に入射する場合は、概ね全反射条件を満たす箇所がどこになるかで決まる。図4において、光線がレンズの周辺に行くにつれて、屈折角が大きくなり、丁度光線 $R_2$ と $R_3$ の間及び光線 $R_9$ と $R_{10}$ の間で全反射条件をむかえる。このときの光線 $R_{2.5}$ 、 $R_{9.5}$ は、レンズの接線方向に射出し、これよりも外側の光線は、一部 $R_2$ 、 $R_{10}$ のように大きく広がるものもあるが全体の光量から見れば、極わずかであり、これよりも少し外側へ行くにつれて、再び $R_1$ 、 $R_{11}$ のように急速に発散光から収束光に転ずる。よって、光線が全反射を起こす迄の範囲(光線 $R_{2.5}$ 、 $R_{9.5}$ の間)が、概ね放出光の拡散角 $\theta_s$ になるとすると、図5、図6のようになる。

【0023】① 切込量 $D \leq r \sin \theta_c$  (いずれかで全反射となる)の場合には、断面が円のときには、曲率半径のいかんによらず、

$$\theta_s \doteq 180^\circ - \theta_c = \sin^{-1}(1/n_1)$$

となるので、所望の $\theta_s$ が与えられたときには、

$$n_1 = 1/(\sin \theta_s)$$

のようにレンズの屈折率 $n_1$ を選ぶことができる。

【0024】② 切込量 $D > r \sin \theta_c > 0$  (常に $\theta < \theta_c$ で全反射なし)の場合には、

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

$$\therefore \theta_2 = \sin^{-1}(n_1 \sin \theta_1)$$

また、 $\theta_1 = \tan^{-1}(x/D)$ より、

拡散角は、

$$\theta_s = 2(\theta_2 - \theta_1) = 2\{\sin^{-1}\{n_1 \sin(\tan^{-1}(x/D))\} - \tan^{-1}(x/D)\}$$

となる。特に、図3(A)のように尖頭部をもつときには、 $2x=P$ より、

$$\theta_s \doteq 2\{\sin^{-1}\{n_1 \sin(\tan^{-1}(P/2D))\} - \tan^{-1}(P/2D)\}$$

となるので、所望の $\theta_s$ が与えられたときには、前記 $\theta_s$ となるように、レンズの屈折率 $n_1$ 、切込量 $D$ 、周期 $P$ を選ぶことができ、選択の自由度が増える。

【0025】図4は、直下型面光源〔図11参照〕の光源直上部のように、レンチキュラーレンズ10の平坦面13に対して、入射角 $=0^\circ$ の平行光束として入射し、凹レンズ部12から放射されるようすを示してある。

【0026】図7は、エッジライト型面光源〔図12参照〕の光等方拡散性層20上にレンチキュラーレンズ10を載置して、平坦面13から光を入射した場合であり、ある角度範囲(図7では、法線Nに対して、 $-40^\circ \sim +40^\circ$ の範囲)に分布した光束が入射したようすを示している〔図13(C)参照〕。

【0027】(光等方拡散性層)図9、図10は、実施例にかかるレンチキュラーレンズと光等方拡散性層との層構成を示す図である。レンチキュラーレンズ10と光等方拡散性層(艶消透明層)20とを積層して使用することができる。この場合には、一旦、光等方拡散性層20によって拡散した光を収束させるために、レンチキュラーレンズ10を観察側、光等方拡散性層20を光源側に配置する必要がある。

【0028】前述したように、レンチキュラーレンズ10は、そのレンズ面12が観察側であっても〔図9(A)、図10(A)〕であっても、光源側であってもよい〔図9(B)、図10(B)参照〕。また、光等方拡散性層20は、シート(又は板)状のもの〔図9参照〕でもよいし、光等方拡散性層20'のように、レンチキュラーレンズ10に直接塗工した膜状のもの〔図10参照〕でもよい。

【0029】光等方拡散性層20、20'は、前記透光性材料に光拡散剤(艶消剤)として、炭酸カルシウム、シリカ、アルミナ、硫酸バリウム等の無機質微粒子、又は、アクリル樹脂等の樹脂ビーズ粒子を分散させたものが用いられ、その粒子の径は、略 $1 \sim 20\mu\text{m}$ 位のものが使用される。光等方拡散性層20は、前記透光性材料に前記光拡散剤を練り込んだ樹脂材料を押出成形、カレンダー成形等でシート化した、単一層として形成ものが使用できる。また、前記透光性材料のシート(又は板)上に、前記透光性材料を結合剤(バインダ)として、これに前記光拡散剤を分散させた塗料を塗工形成して使った2層構成物でもよい。さらに、前記透光性材料のシート(又は板)の表面を、サンドブラスト、エンボス賦型加工等によって、中心線平均粗さ $1 \sim 20\mu\text{m}$ の微小凹凸(砂目等)を形成したものである。

【0030】（直下型の面光源の実施例）図11は、本発明による面光源の第1の実施例（直下型）を示した断面図である。直下型の面光源30は、ケース31内に、蛍光灯などの線光源32が設けられており、ケース31の開口側に、光等方拡散性層20及びレンチキュラーレンズ10とを設けたものである。

【0031】（エッジライト型の面光源の実施例）図12は、本発明による面光源の第2の実施例（エッジライト型）を示す展開的斜視図、図13は、導光板の特性を説明するための図である。エッジライト型の面光源40は、導光板41の下面に、反射層42が形成されており、導光板41の上面に、光等方拡散性層20及びレンチキュラーレンズ10が配置されている。また、導光板41の側端面の両側には、それぞれ光源43、反射膜44、照明カバー45が設けられている。

【0032】導光板41の入射角 $i$ が臨界角 $i_c$ よりも大きい場合には、図13（A）に示すように、光線は、導光板41内を全反射しながら伝播するのみであって、放出面41aからの透過光はない。一方、入射角 $i$ が臨界角 $i_c$ よりも小さい場合には、図13（B）に示すように、導光板41の放出面41aの側界面において、光線の一部は、反射（導光板41内を伝播）し、残りは透過して放出される。また、実際の導光板41では、図13（C）に示すように、他方の端面に光源43'を置か、または光反射層42'を設けることにより、導光板41の内部を光線が双方向に伝播し法線に対して左右対称な $\pm\theta$ 方向に光が放出される。

【0033】（光反射層の実施例）図14は、エッジライト型の面光源に用いられる光反射層の実施例を示す図である。光反射層42は、光を拡散反射させる性能を持つ層であって、以下のように構成することができる。

① 図14（A）のように、導光板41の片面に、高隠蔽性かつ白色度の高い顔料、例えば、二酸化チタン、アルミニウム等の粉末を分散させた白色層42Aを塗装などによって形成する。

② 図14（B）のように、導光板41の片面に、サンドブライト加工、エンボス加工等によって艶消微細凹凸41aを形成し、さらに、アルミニウム、クロム、銀等のような金属をメッキ又は蒸着等して、金属薄膜層42Bを形成する。

③ 図14（C）のように、図14（A）と同様な白色層42A'（ただし、隠蔽性は低くてもよい）に、金属薄膜層42Bを形成する。

④ 図14（D1）、（D2）のように、網点状の白色層42A''を形成し、光源43から遠ざかるに従って面積率を増やして、光源43の光量が減衰するのを補正するようにしてもよい。

【0034】図11、図12に示した面光源30、40は、公知の透過型の液晶表示素子の背面に配置することによって、液晶表示装置として使用することができる。また、透過型の液晶表示素子の他に、エレクトロクロミック表示素子などの背面光源を必要とする素子に適用することができる。

【0035】（透過測定）本件発明者等は、製造例1、2及び比較例1に示すようなレンチキュラーレンズを作製し、図12に示すエッジライト型面光源40に、レンズ面12等が上（外側）になるようにして、光等方拡散性層20の上に載置し、レンズ面12等から放出される光の輝度の角度分布を測定した。なお、比較例2として、光等方拡散性層20のみの場合も測定した。

#### 【0036】製造例1

形状 ; 図1（又は図2）、断面は円形

曲率半径 $r$  ;  $35\mu\text{m}$

周期 $P$  ;  $59\mu\text{m}$

切込量 $D$  ;  $15\mu\text{m}$

材料 ; アクリル樹脂

屈折率 $n_1$  ; 1.5

#### 製造例2

形状 ; 図3（B）、断面は円形

曲率半径 $r$  ;  $100\mu\text{m}$

周期 $P$  ;  $300\mu\text{m}$

切込量 $D$  ;  $100\mu\text{m}$

材料 ; アクリル樹脂

屈折率 $n_1$  ; 1.5

#### 比較例1

形状 ; 頂角 $=90^\circ$ 、両底角 $=45^\circ$ の3角柱プリズム型のレンチキュラーレンズ〔図15（B）〕

周期 $P$  ;  $100\mu\text{m}$

材料 ; アクリル樹脂

屈折率 $n_1$  ; 1.5

#### 比較例2

レンチキュラーレンズを用いずに、光等方拡散性層20〔図15（A）〕のみによって測定した。

【0037】製造例1、2及び比較例1、2の測定結果を、図8の曲線A、B、C、Dにそれぞれ示してある。これらの測定結果に基づいて、以下の表1が得られる。

表1（測定結果）

	半値角 $\theta_H$ [°]	サイドローブ比 [%]	法線方向輝度比 [%]
製造例1 ;	38	11	111.2
製造例2 ;	35	22	108.5
比較例1 ;	34	26	135.0
比較例2 ;	37	0	100.0（基準）

散光が法線方向近傍の所定範囲（通常、半値角  $\theta_H = 30^\circ \sim 90^\circ$  程度）に集光されていることが判る。また、比較例1の90度頂角の三角柱プリズム型のレンチキュラーレンズと比較して、サイドロブ光の発生が少ないことが判る。

#### 【0039】

【発明の効果】以上詳しく説明したように、本発明によれば、レンチキュラーレンズのレンズ面の単位凹レンズ部の形状パラメータ（例えば、曲率半径、周期、切込量及び屈折率など）によって、所望の角度分布の光を拡散することができる（請求項1，2）。

【0040】従って、請求項3のように、光等方拡散性層と組み合わせることにより、光等方拡散性層のみの場合と比較して、拡散光が法線方向に対して所望の角度範囲に集光されるために、所定の角度範囲においては、同じ消費電力であっても、より高輝度となり、逆に、同じ輝度を得るためには、より低消費電力で足りる。

【0041】また、斜め方向から接線方向に放射される光エネルギーが減少するので、迷光の発生がより少なくなる。さらに、従来の90度頂角の三角柱プリズム型のレンチキュラーレンズと比較して、サイドロブ光の発生が少なくなり、迷光の発生がより少ない。

#### 【図面の簡単な説明】

【図1】本発明によるレンチキュラーレンズの第1の実施例を示す斜視図である。

【図2】本発明によるレンチキュラーレンズの第2の実施例を示す断面図である。

【図3】実施例によるレンチキュラーレンズの単位凹レンズ部の形状を示す断面図である。

【図4】実施例によるレンチキュラーレンズを通過する

光線の軌跡を示す図である。

【図5】実施例によるレンチキュラーレンズを通過する光線の軌跡を示す図である。

【図6】実施例によるレンチキュラーレンズを通過する光線の軌跡を示す図である。

【図7】実施例によるレンチキュラーレンズを通過する光線の軌跡を示す図である。

【図8】本発明によるレンチキュラーレンズの実施例の透過特性を示す線図である。

【図9】実施例にかかるレンチキュラーレンズと光等方拡散性層との層構成を示す図である。

【図10】実施例にかかるレンチキュラーレンズと光等方拡散性層との層構成を示す図である。

【図11】本発明による面光源の第1の実施例（直下型）を示した断面図である。

【図12】本発明による面光源の第2の実施例（エッジライト型）を示す展開的斜視図である。

【図13】図12に示す導光板の特性を説明するための図である。

【図14】エッジライト型の面光源に用いられる光反射層の実施例を示す図である。

【図15】エッジライト型の面光源の従来例を示す図である。

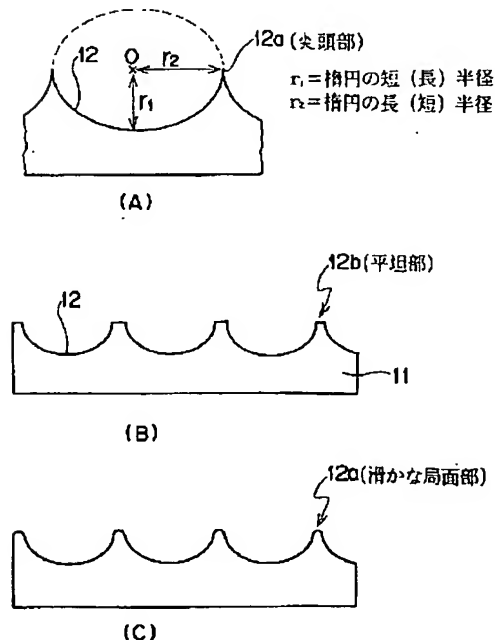
#### 【符号の説明】

- 10 レンチキュラーレンズ
- 11 透光性基材
- 12 レンズ面
- 13 平坦面
- 20 光等方拡散性層

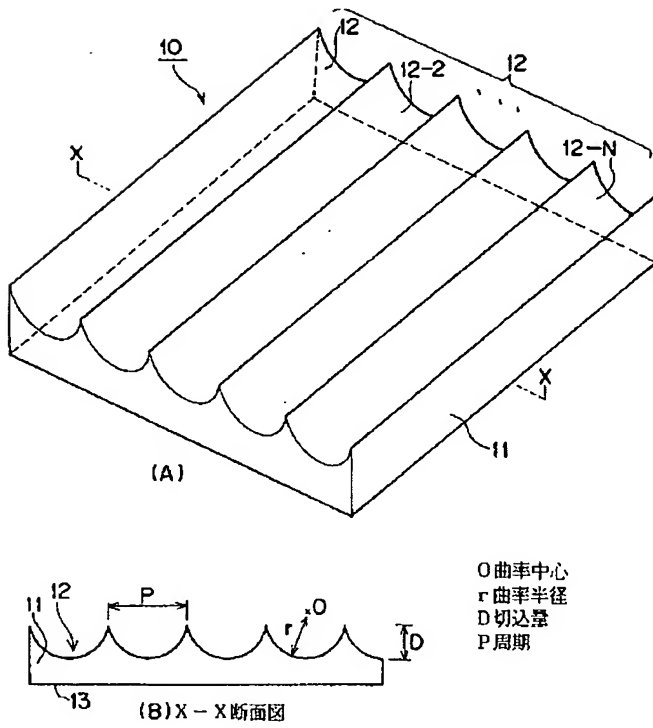
【図2】



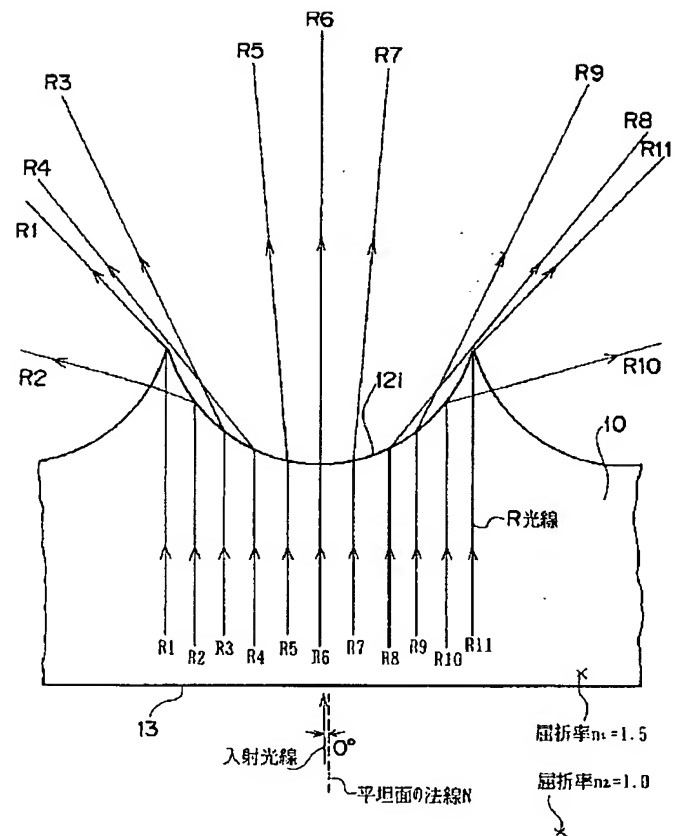
【図3】



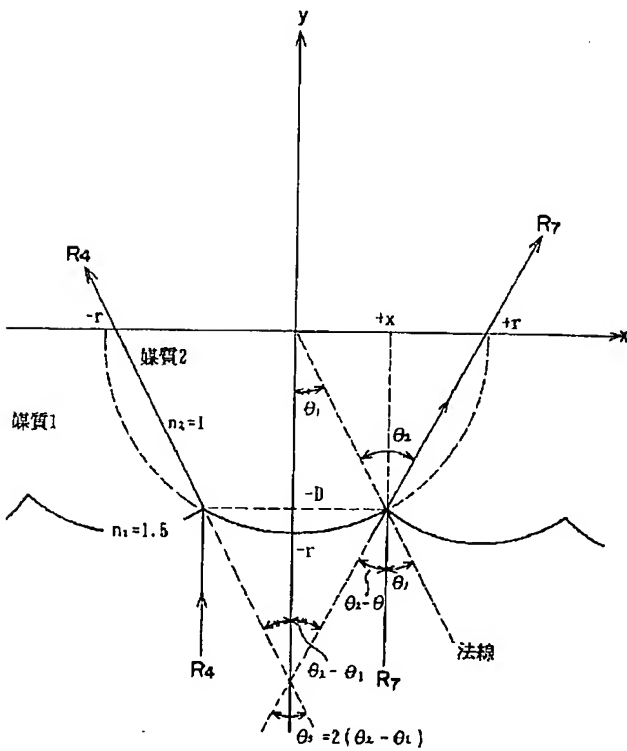
【図1】



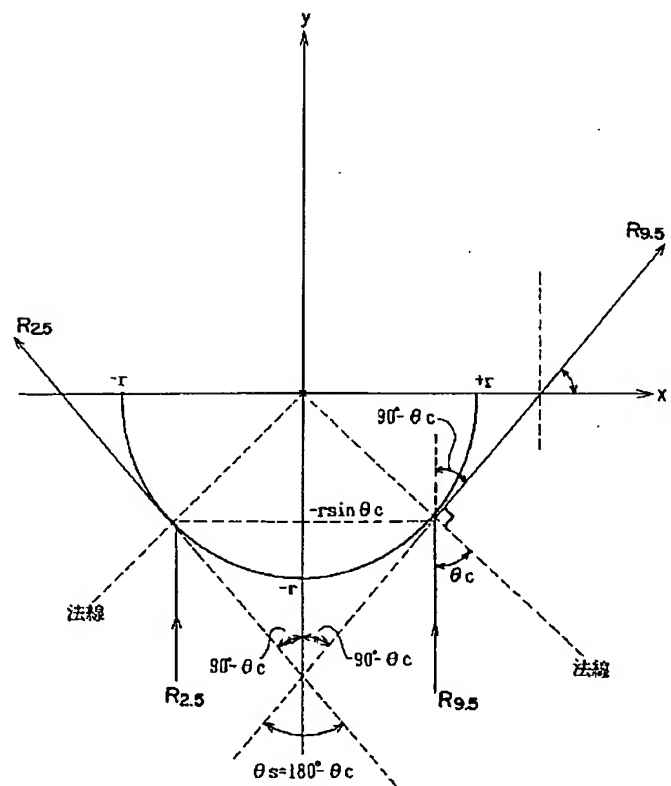
【図4】



【図5】

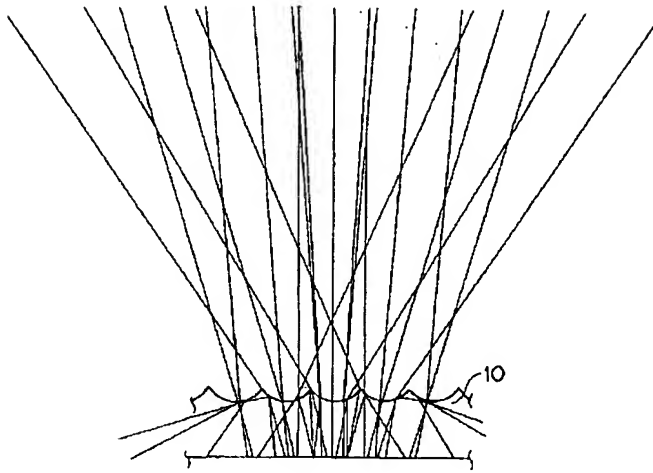


【図6】

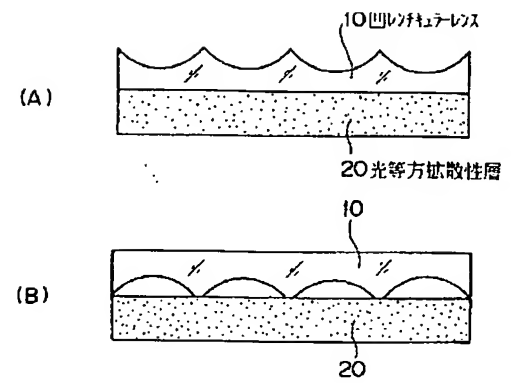




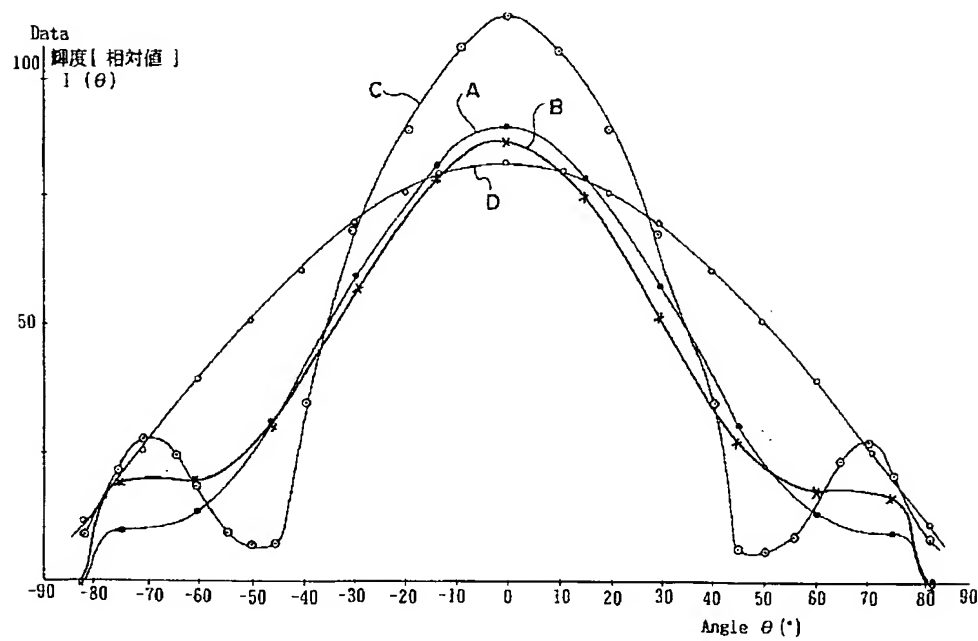
【図7】



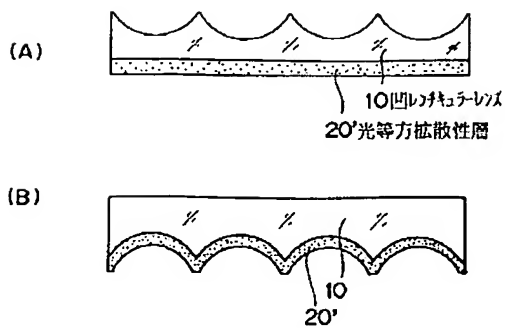
【図9】



【図8】

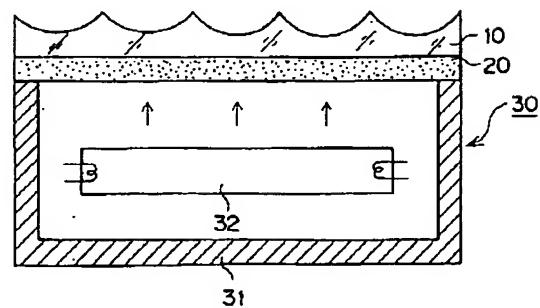


【図10】



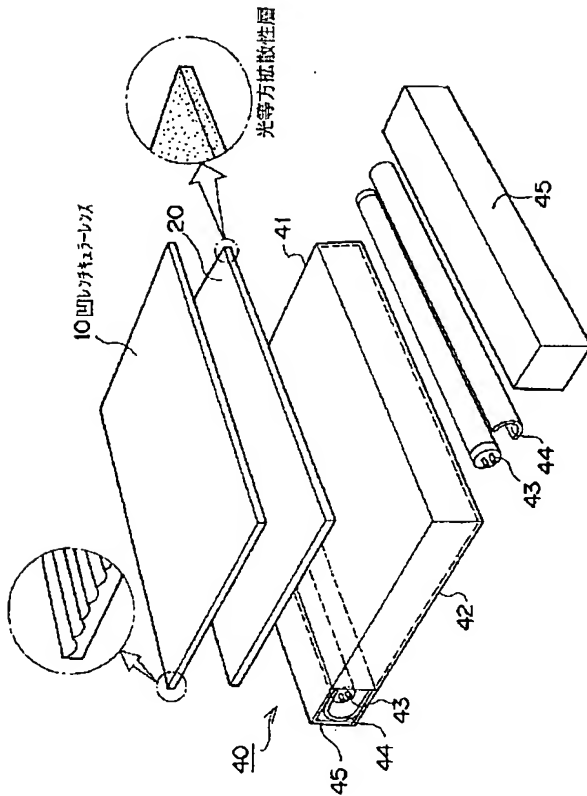
【図11】

(直下型面光源)

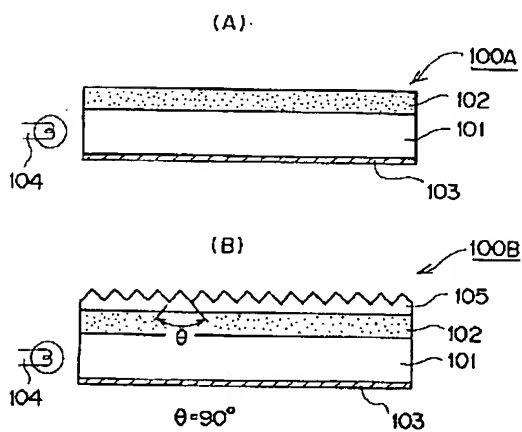


【図12】

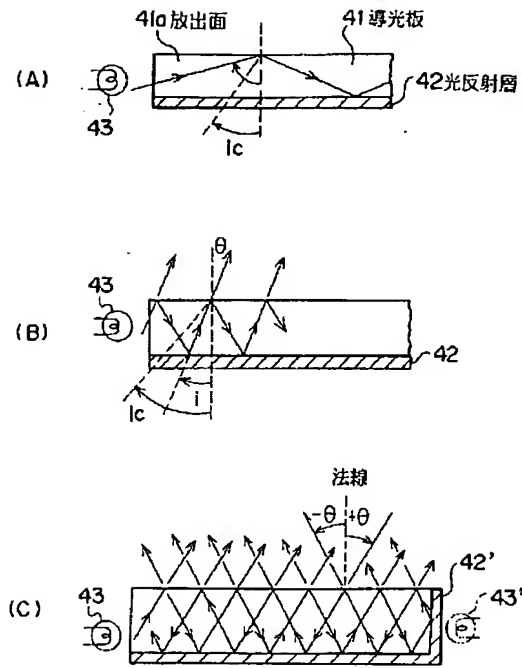
(エッジライト型面光源)



【図15】



【図13】



【図14】

